

Oxidation Phenomena in Advanced High Strength Steels

Project ZCO-62 International Zinc Association

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Predicting mixed oxide formation

- In order to predict oxide formation in multi-element steel alloys a thermodynamic database is being developed that needs validation
- Oxidation experiments with Mn steels with Al, Si and Cr additions have been done
- The resulting oxide precipitates were analyzed
- A comparison with thermodynamic predictions is made
- Modelling of the formation of single oxides is done
- Modelling of the formation of mixed oxides is in progress

1.

*Oxidation experiments with Mn
Steel Alloyed with Al, Si and Cr*

Mn steel alloys and annealing conditions

Sample (wt%)	C	Mn	Cr	Si	Al
A	0.103	1.7	-	0.049	0.002
B	0.099	1.8	0.53	0.25	0.003
C	0.101	1.8	1.02	0.26	0.019
D	0.102	2.8	0.55	0.25	0.005
E	0.177	1.8	-	0.15	0.95
F	0.202	1.8	-	0.97	0.90
G	0.104	1.9	-	0.94	0.017

Annealing atmosphere: N₂ with 5 vol.% H₂

Temperature (°C)	Time (min)	Dew point (°C)	P _{O2}	Code
950	60	-45	8.0×10 ⁻²²	1
950	60	-31	1.8×10 ⁻²⁰	2
950	60	-10	1.0×10 ⁻¹⁸	3
950	60	+10	2.3×10 ⁻¹⁷	4

Mn steel alloys and annealing conditions

Sample (mol%)	C	Mn	Cr	Si	Al
A	0.48	1.7	-	0.097	0.004
B	0.46	1.8	0.57	0.49	0.006
C	0.47	1.8	1.09	0.51	0.039
D	0.47	2.8	0.59	0.49	0.01
E	0.81	1.8	-	0.29	1.93
F	0.91	1.8	-	1.88	1.81
G	0.48	1.9	-	1.84	0.03

Annealing atmosphere: N₂ with 5 vol.% H₂

Temperature (°C)	Time (min)	Dew point (°C)	P_{O2}	Code
950	60	-45	8.0×10^{-22}	1
950	60	-31	1.8×10^{-20}	2
950	60	-10	1.0×10^{-18}	3
950	60	+10	2.3×10^{-17}	4

Activity of alloying element at 950 ° C, calculated with “Thermocalc”

Sample	C	Mn	Cr	Si	Al	Fe
A		1.2×10^{-2}	-	2.9×10^{-9}	2.4×10^{-8}	0.977
B		1.2×10^{-2}	5.3×10^{-3}	1.5×10^{-8}	3.8×10^{-8}	0.968
C		1.2×10^{-2}	1.0×10^{-2}	1.5×10^{-8}	2.4×10^{-7}	0.962
D		2.0×10^{-2}	5.6×10^{-3}	1.3×10^{-8}	6.6×10^{-8}	0.958
E		1.3×10^{-2}	-	1.3×10^{-8}	1.5×10^{-5}	0.947
F		1.1×10^{-2}	-	1.1×10^{-7}	1.9×10^{-5}	0.925
G		1.1×10^{-2}	-	7.2×10^{-8}	2.7×10^{-7}	0.957

Activities of all alloying elements smaller than that of Mn

2.

SEM cross-section analysis
Effect of dew point

SEM cross-section observation: Fe-Mn

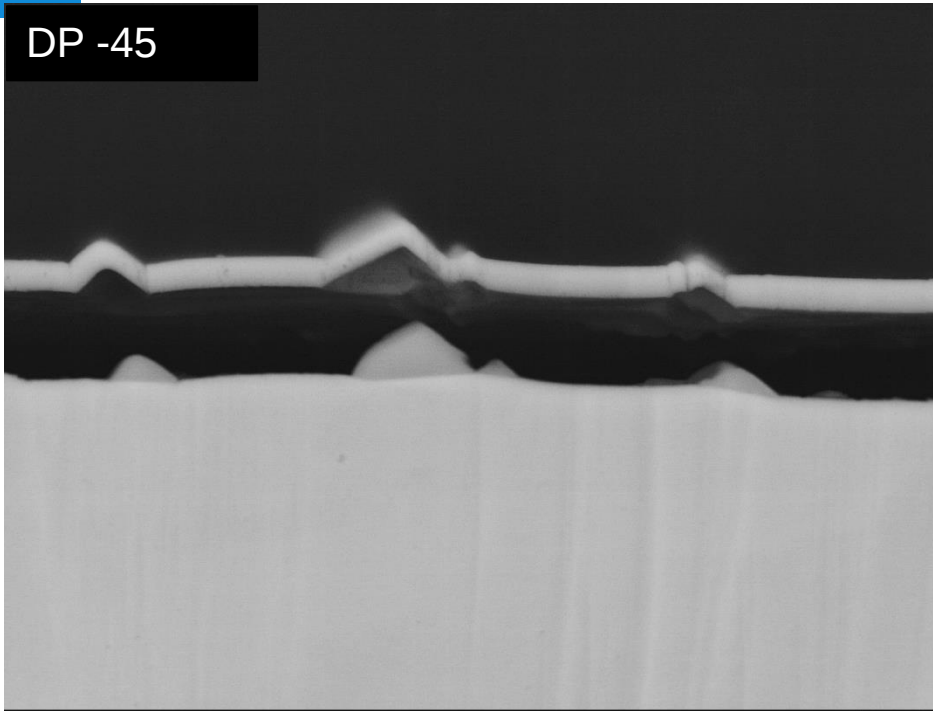
Annealing condition in N₂ with 5 vol.% H₂

Sample composition (mol%):

Dew point (° C)	Temperature (° C)	P _{O2}
-45	950	8.0×10^{-22}
+10		2.3×10^{-17}

	C	Mn	Si	Al
Sample A	0.48	1.72	0.097	0.004

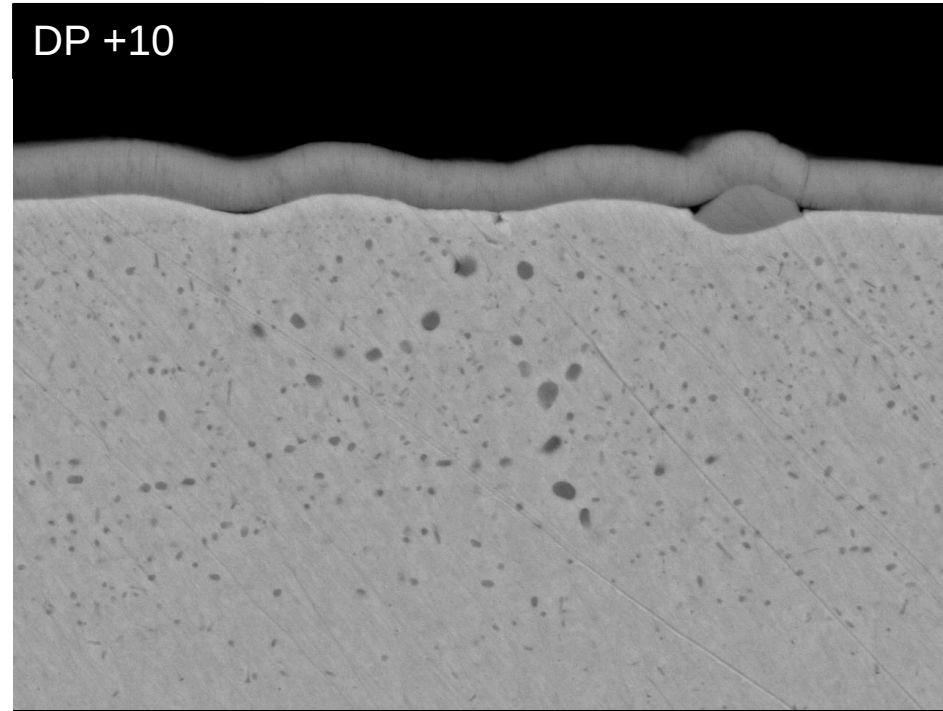
DP -45



TU Delft BSE 15.0kV X8,000 WD 10.1mm 1μm

External MnO

DP +10



TU Delft BSE 15.0kV X6,000 WD 10.1mm 1μm

Internal MnO

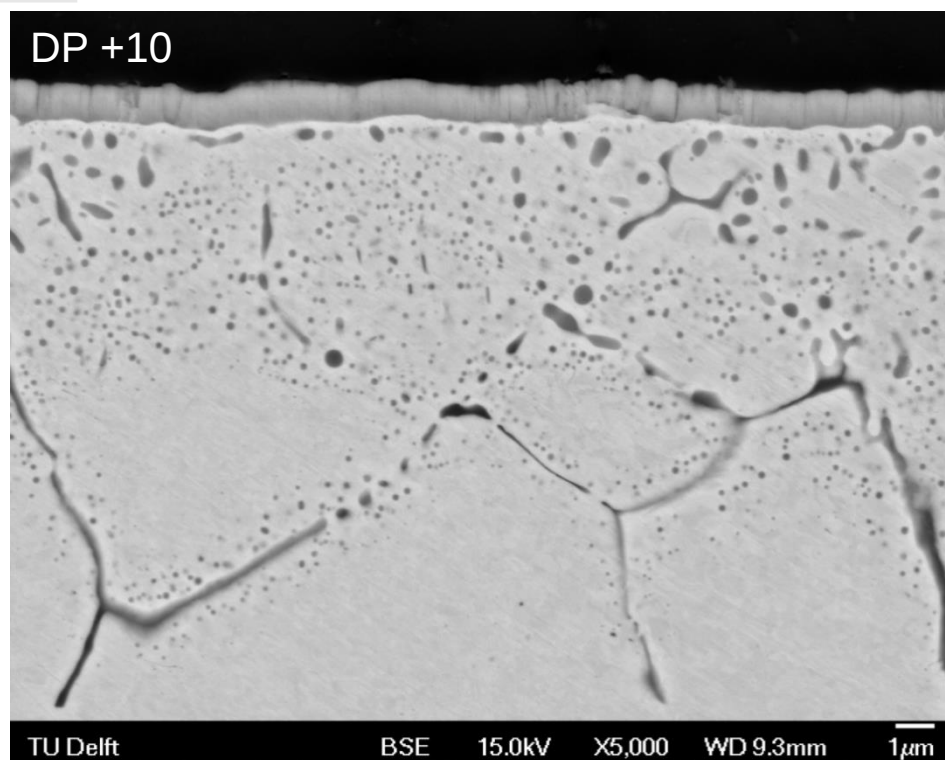
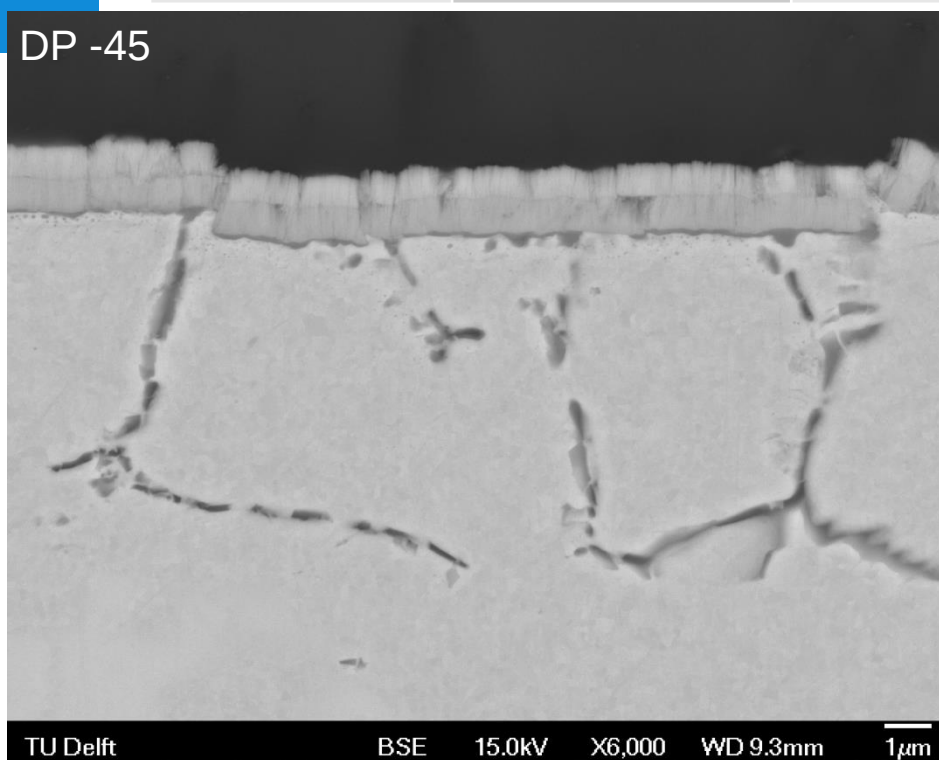
SEM cross-section observation: Fe-Mn-Si

Annealing condition in N₂ with 5 vol.% H₂

Dew point (° C)	Temperature (° C)	P _{O2}
-45	950	8.0×10^{-22}
+10		2.3×10^{-17}

Sample composition (mol%):

	C	Mn	Si	Al
Sample G	0.48	1.91	1.84	0.03



Si promotes Mn₂SiO₄ formation along grain boundaries

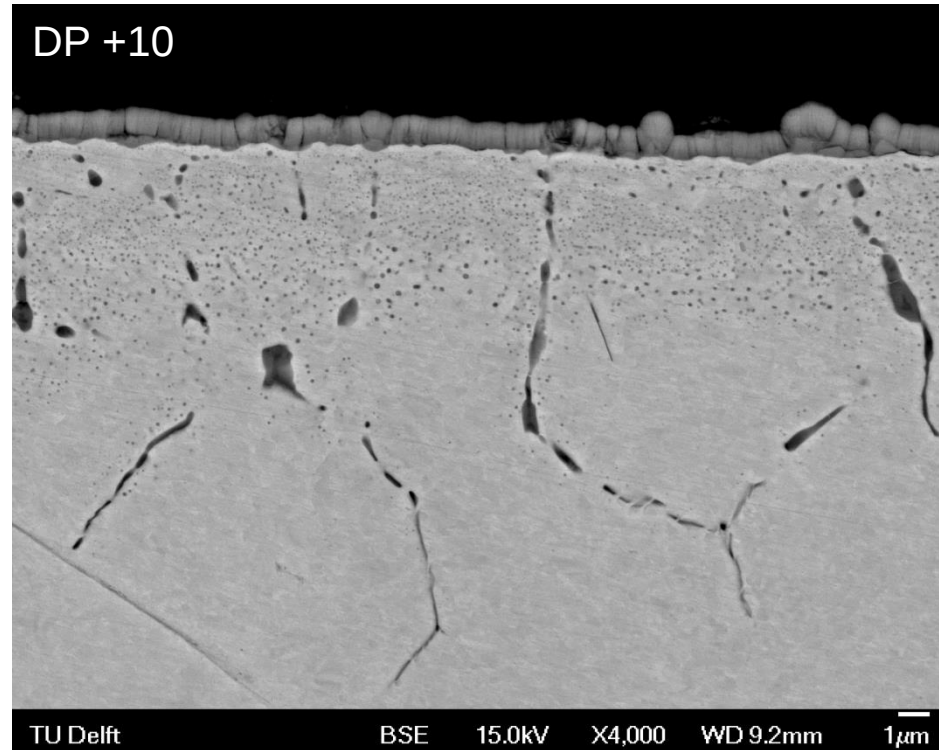
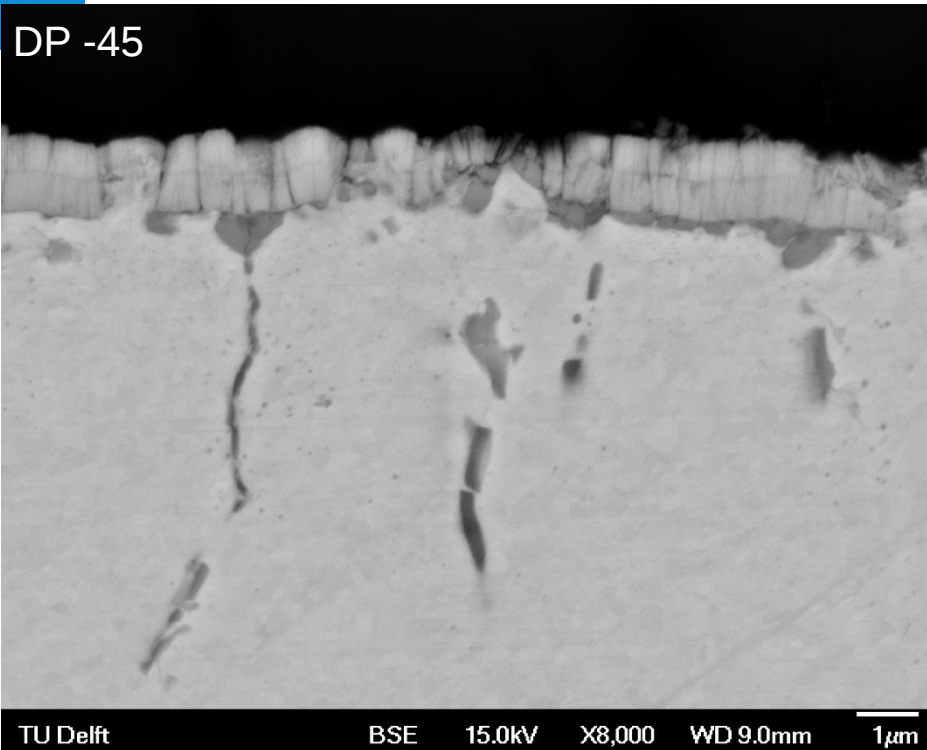
SEM cross-section observation: Fe-Mn-Cr-(Si)

Annealing condition in N₂ with 5 vol.% H₂

Sample composition (mol%):

Dew point (° C)	Temperature (° C)	P _{O2}
-45	950	8.0×10^{-22}
+10		2.3×10^{-17}

	C	Mn	Cr	Si	Al
Sample C	0.47	1.82	1.09	0.51	0.039



Cr forms mainly internal MnCr₂O₄

Additional Si promotes Mn₂SiO₄ along grain boundaries

SEM cross-section observation: Fe-Mn-Al-(Si)

Annealing condition in N₂ with 5 vol.% H₂

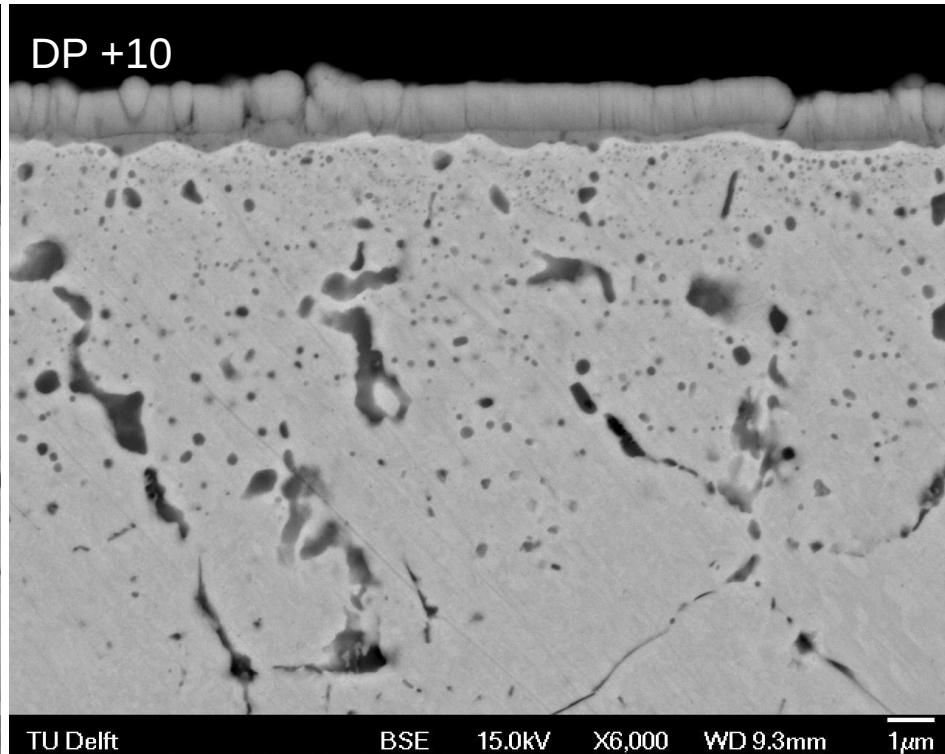
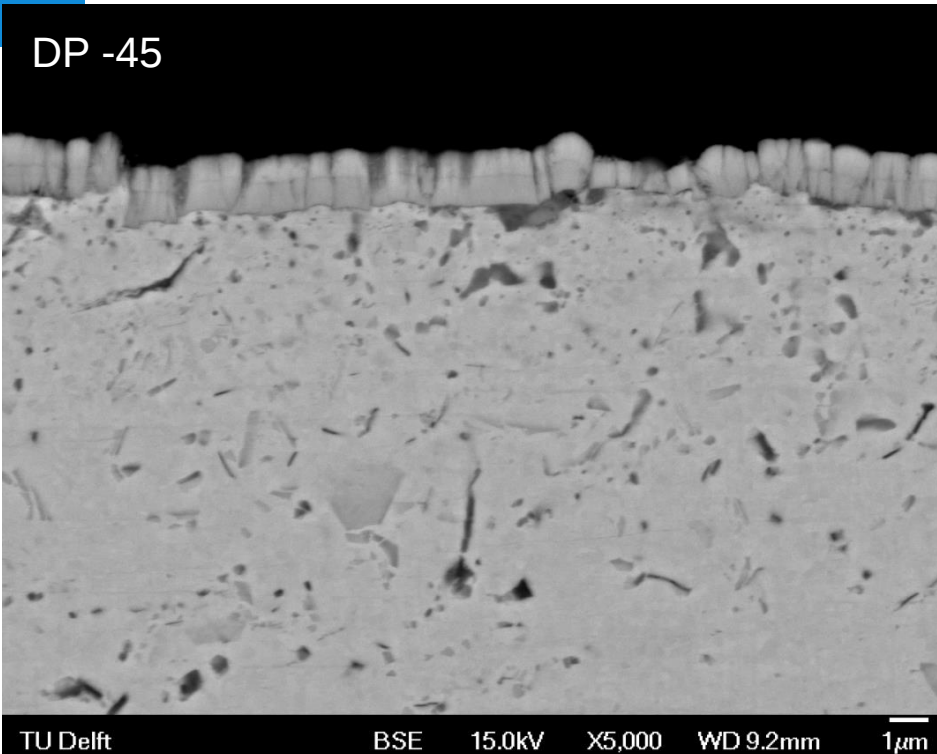
Sample composition (mol%):

Dew point (° C)	Temperature (° C)	P _{O2}
-45	950	8.0×10^{-22}
+10		2.3×10^{-17}

	C	Mn	Si	Al
Sample E	0.81	1.8	0.29	1.93

DP -45

DP +10



At low DP AlN is formed, but suppressed with increasing DP
Al promotes formation of external MnO and formation of internal MnAl₂O₄

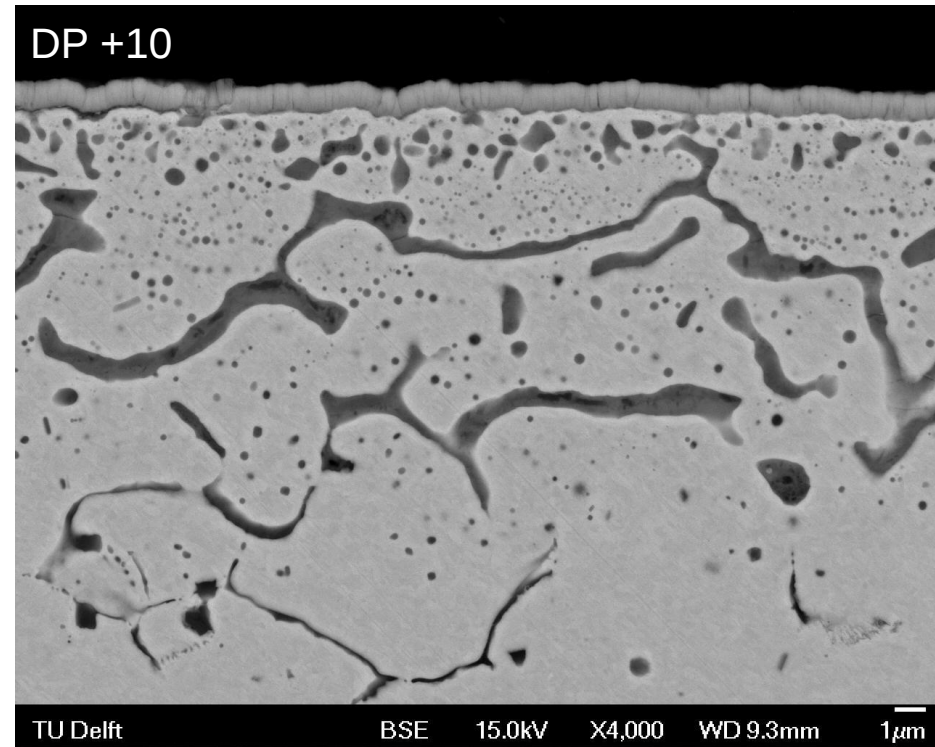
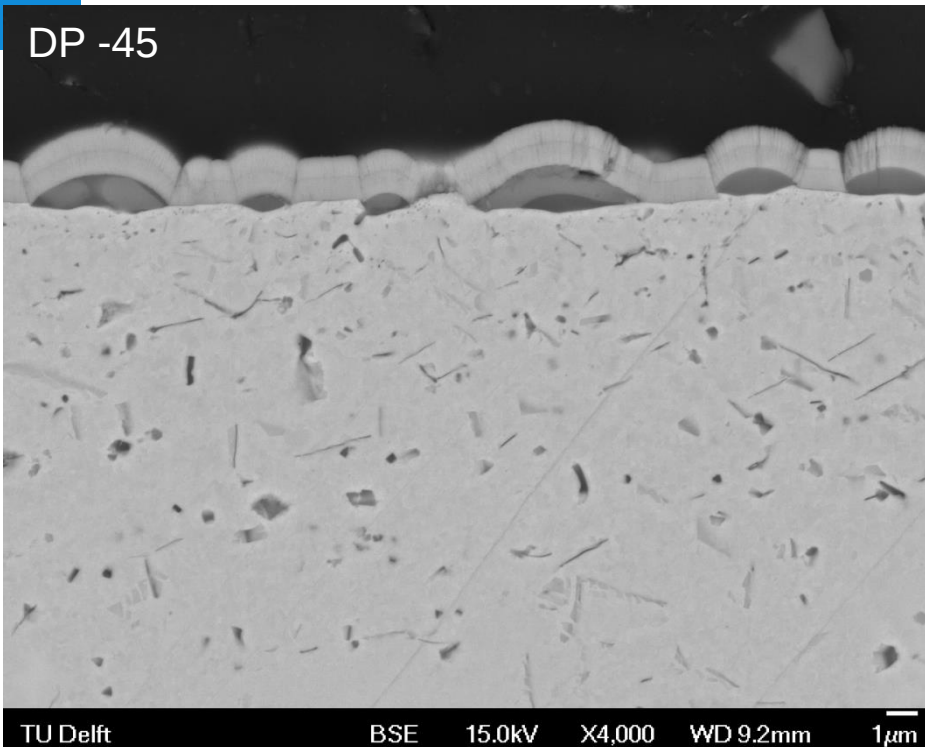
SEM cross-section observation: Fe-Mn-Al-Si

Annealing condition in N₂ with 5 vol.% H₂

Sample composition (mol%):

Dew point (° C)	Temperature (° C)	P _{O2}
-45	950	8.0×10^{-22}
+10		2.3×10^{-17}

	C	Mn	Si	Al
Sample F	0.91	1.78	1.88	1.81



Both MnAl₂O₄ and Mn₂SiO₄ are formed, inside grains as well as along grain boundaries

3.

*XRD analysis & thermodynamic
predictions of oxide formation*

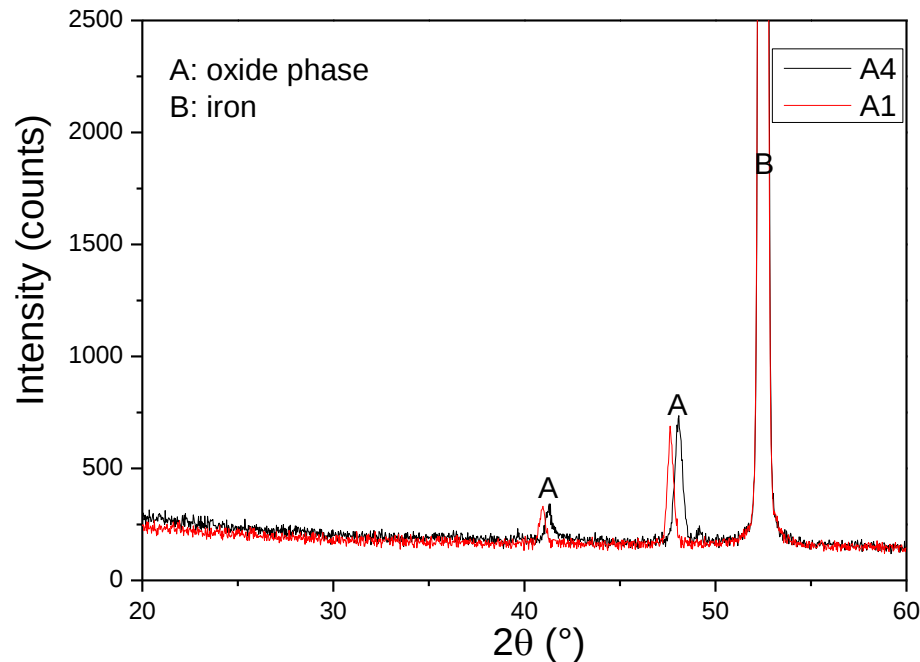
XRD analysis: Fe-Mn

Annealing condition in N₂ with 5 vol.% H₂

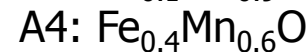
Sample	Dew point (°C)	Temperature (°C)	P _{O2}
A1	-45	950	8.0×10^{-22}
A4	+10		2.3×10^{-17}

Sample composition (mol%):

	C	Mn	Si	Al
Sample A	0.48	1.72	0.097	0.004



Fe-Mn mixed oxide is formed:

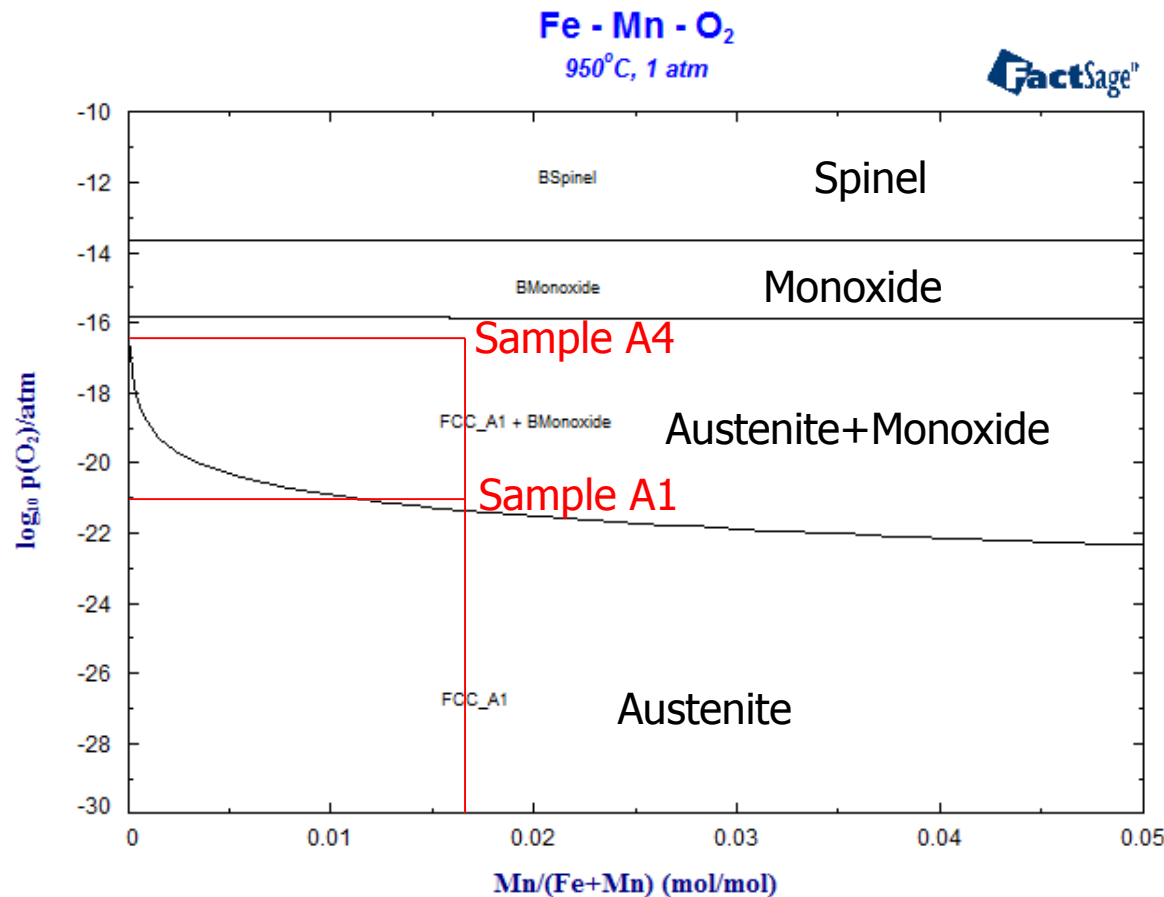


The dew point for sample A4 is still lower than the critical value for the formation of FeO

The (Mn,Fe)O oxide phase has rock-salt crystal structure

Prediction of oxides formation: Fe-Mn

Phase diagram of Fe-Mn alloy in O₂ environment



Database: FactPS, Ftoxid, FSstel

Solution Phases selected in calculation:
BSpinel, BMonoxide, FCC_A1

BSpinel is a solution of Fe₃O₄, MnFe₂O₄, FeMn₂O₄ with cubic crystal structure

BMonoxide is a solution of Fe₂O₃, FeO, MnO, Mn₂O₃ with rock-salt crystal structure

The amount of Fe in (Mn,Fe)O monoxide phase can be computed, which increases with dew point

XRD results agree with "Factsage" calculation

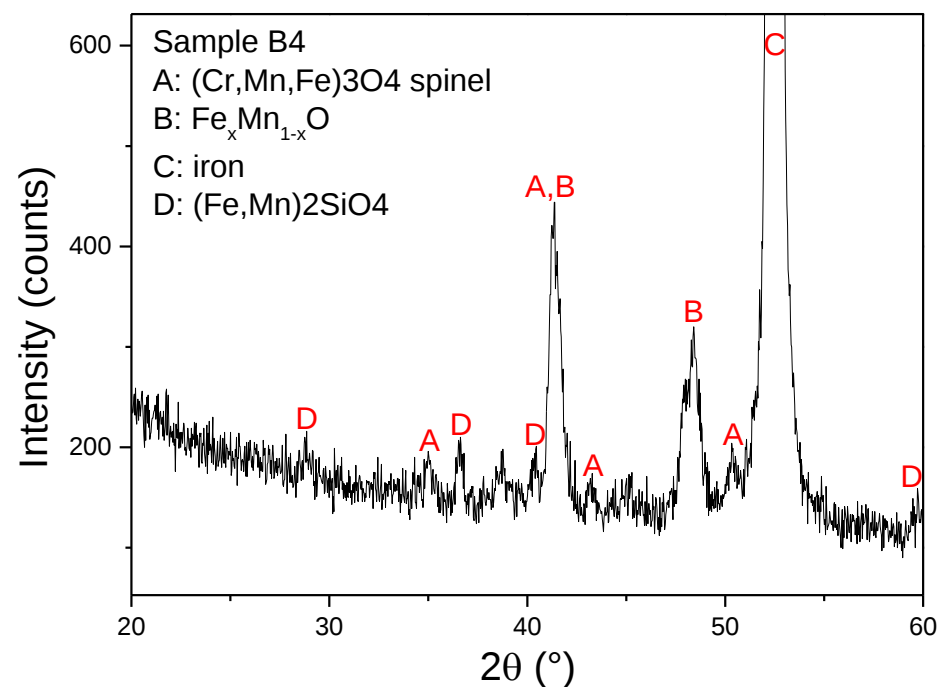
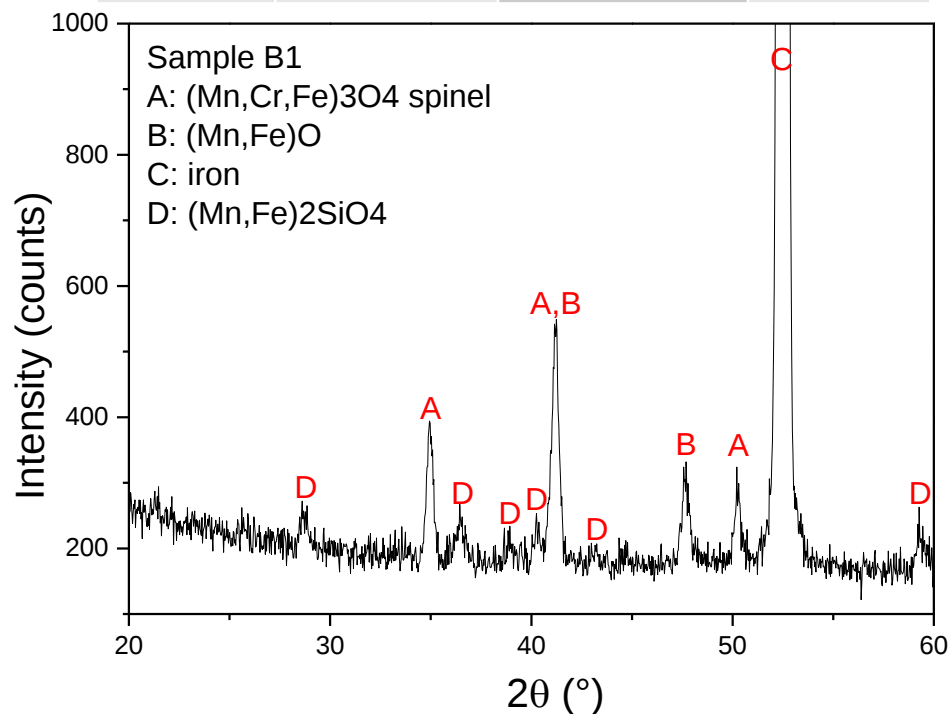
XRD analysis: Fe-Mn-Cr-(Si)

Annealing condition in N₂ with 5 vol.% H₂

Sample	Dew point (°C)	Temperature (°C)	P _{O2}
B1	-45	950	8.0×10^{-22}
B4	+10		2.3×10^{-17}

Sample composition (mol%):

	C	Mn	Cr	Si	Al
Sample B	0.46	1.82	0.57	0.49	0.006



Addition of Cr leads to formation of (Mn,Cr,Fe)₃O₄ cubic spinel oxide

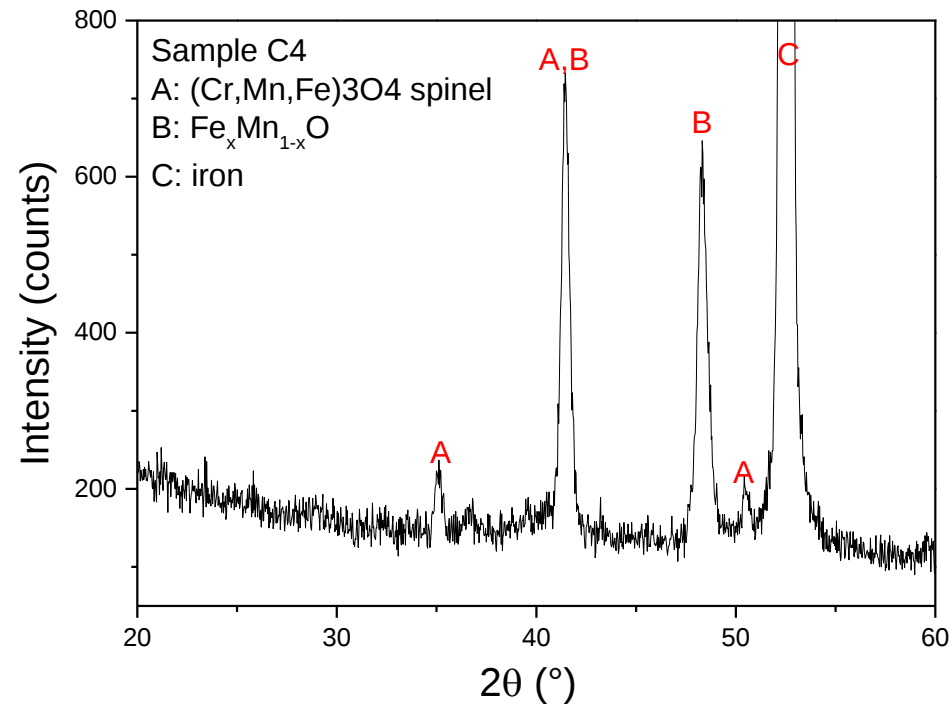
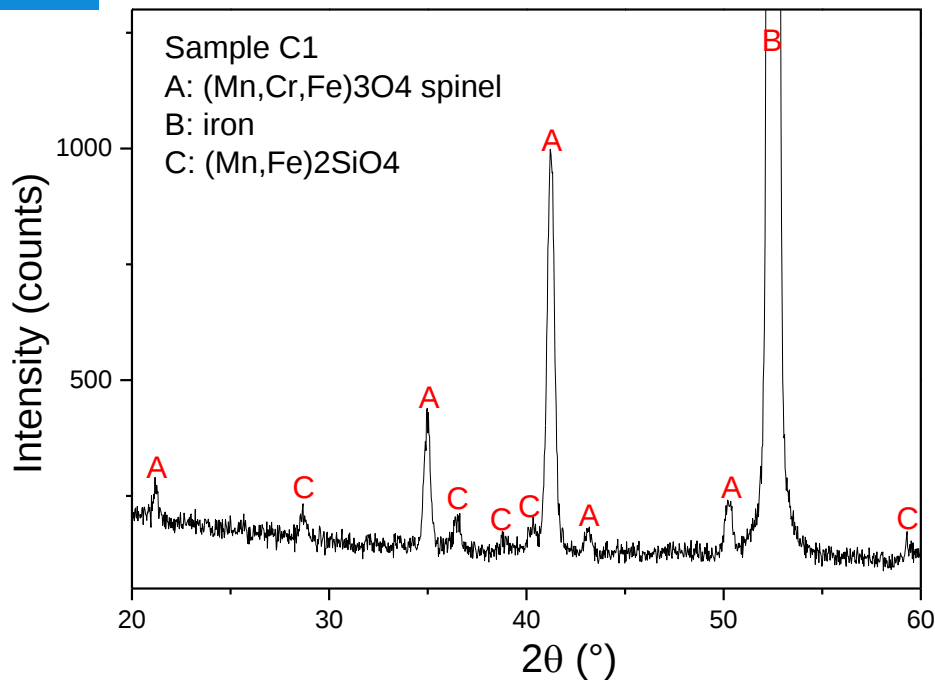
XRD analysis: Fe-Mn-Cr-(Si)

Annealing condition in N₂ with 5 vol.% H₂

Sample	Dew point (°C)	Temperature (°C)	P _{O2}
C1	-45	950	8.0×10^{-22}
C4	+10		2.3×10^{-17}

Sample composition (mol%):

	C	Mn	Cr	Si	Al
Sample C	0.47	1.82	1.09	0.51	0.039



Again addition of Cr leads to the formation of (Mn,Cr,Fe)₃O₄ cubic spinel oxide
Higher Cr concentration does not change type of oxides formed

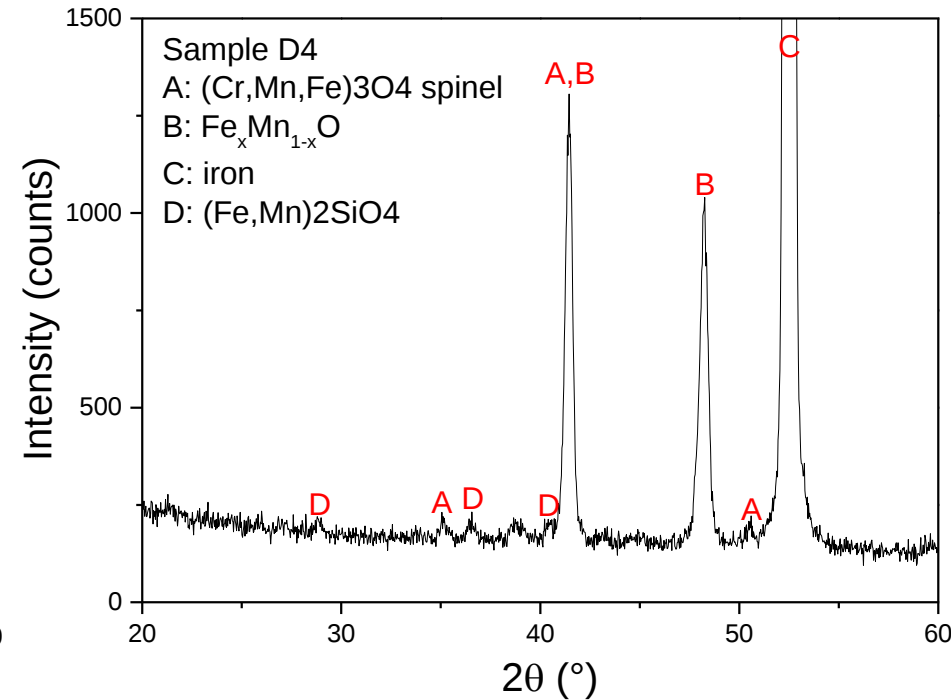
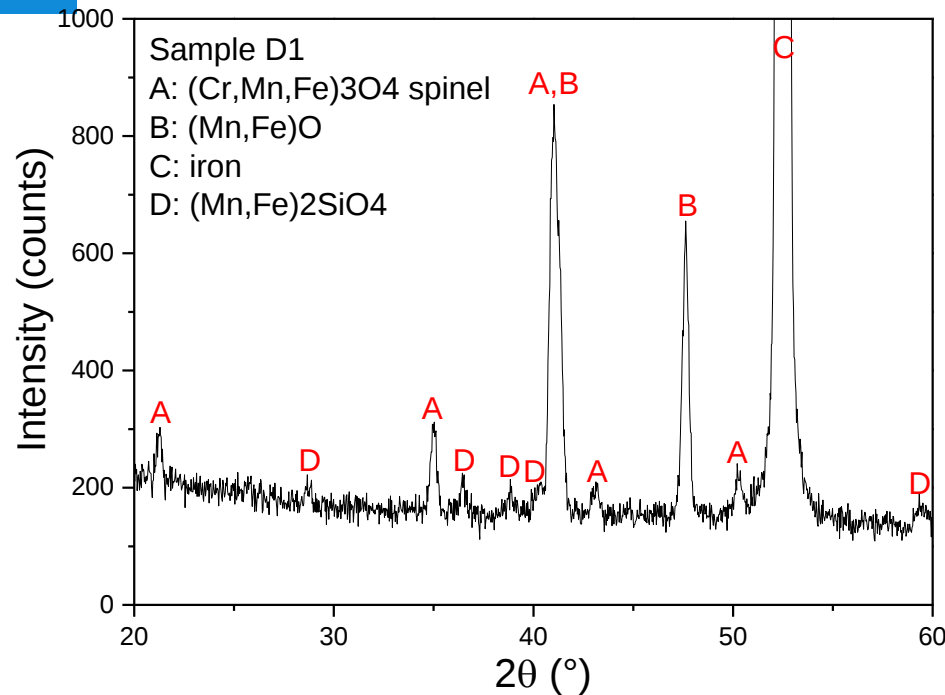
XRD analysis: Fe-Mn-Cr-(Si)

Annealing condition in N₂ with 5 vol.% H₂

Sample	Dew point (°C)	Temperature (°C)	P _{O2}
D1	-45	950	8.0×10 ⁻²²
D4	+10		2.3×10 ⁻¹⁷

Sample composition (mol%):

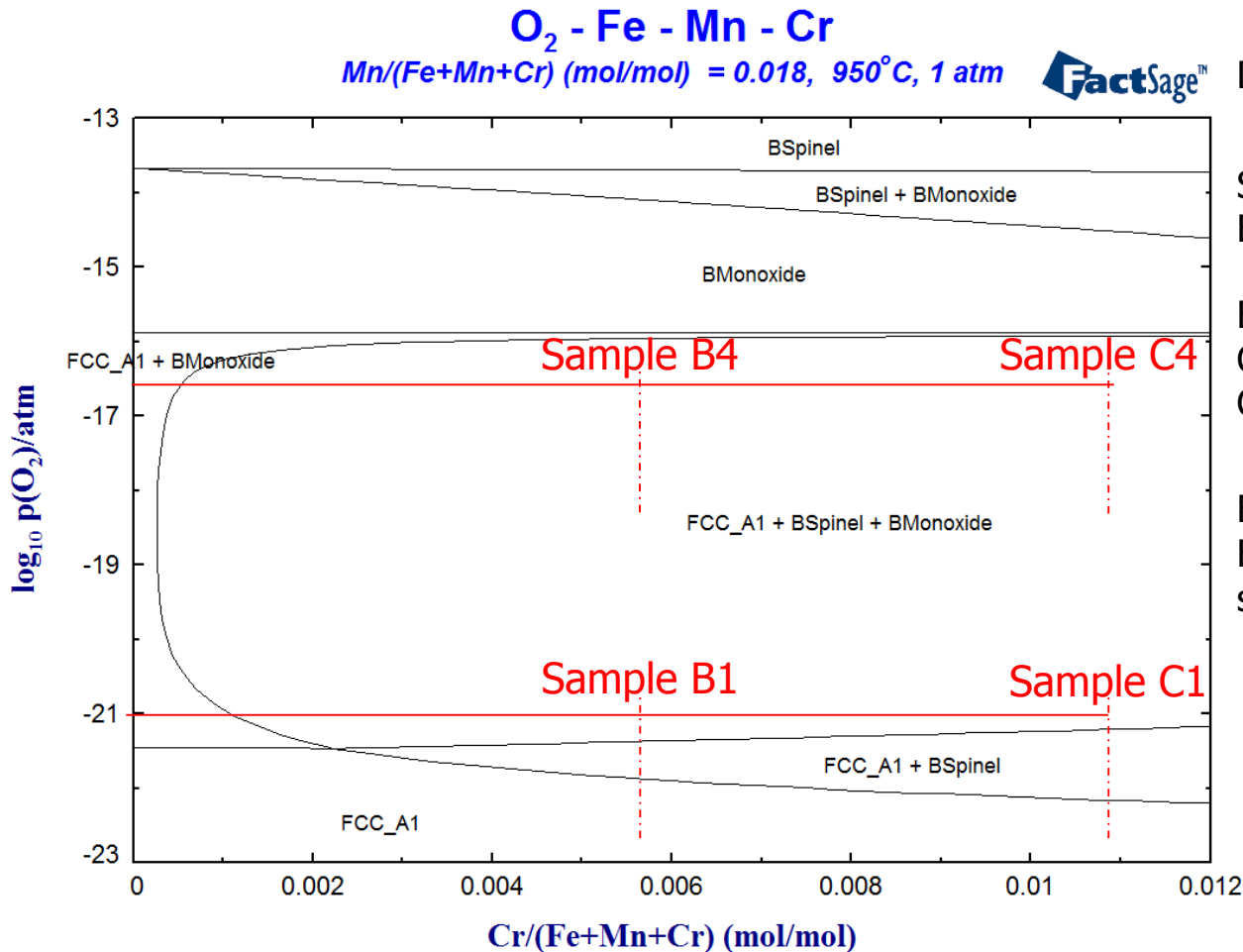
	C	Mn	Cr	Si	Al
Sample D	0.47	2.83	0.58	0.49	0.001



Again addition of Cr leads to the formation of (Mn,Cr,Fe)₃O₄ cubic spinel oxide
Higher Mn concentration does not change type of oxides formed

Prediction of oxides formation: Fe-Mn-Cr

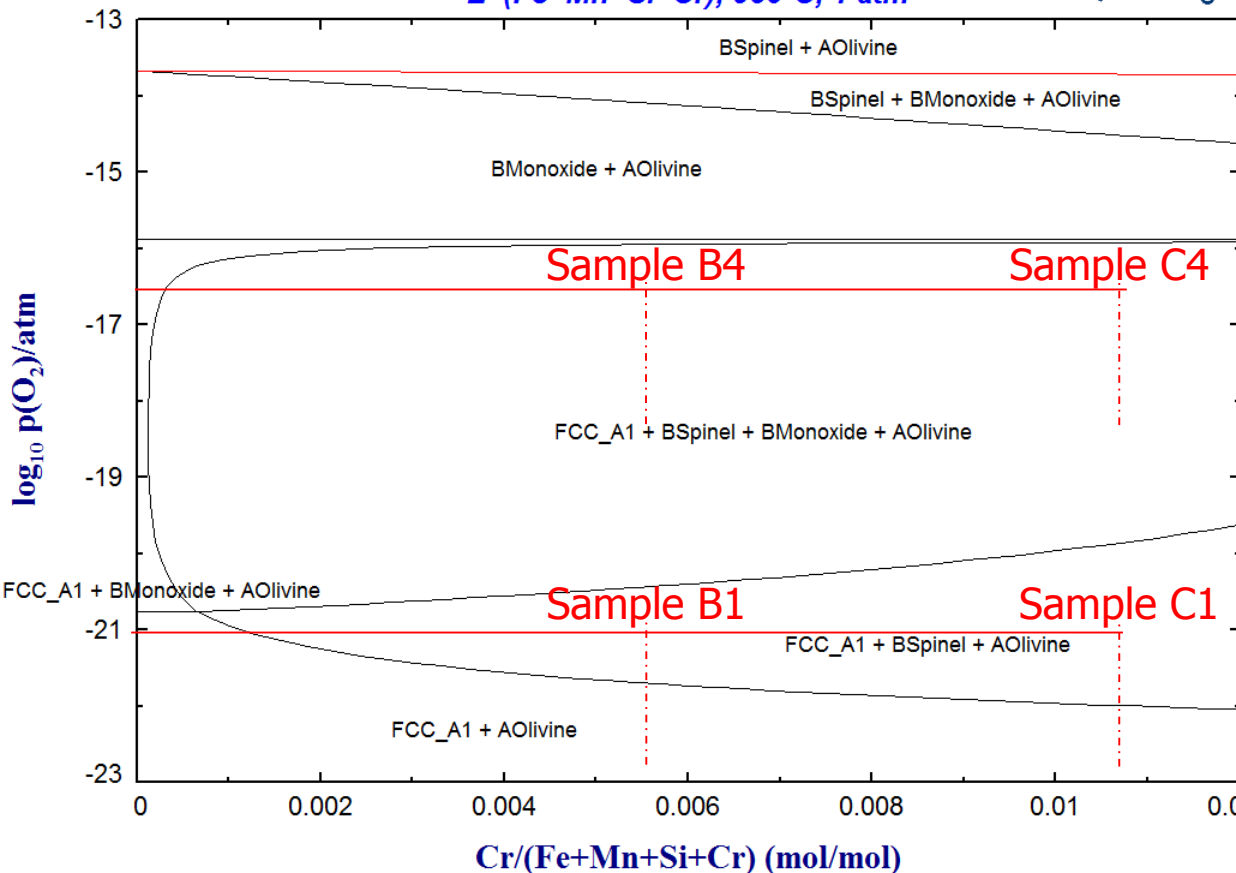
Phase diagram of Fe-1.8Mn-Cr alloy in O₂ environment



Prediction of oxides formation: Fe-Mn-Cr-Si

Phase diagram of Fe-1.8Mn-0.5Si-Cr alloy in O₂ environment

Fe - Mn - O₂ - Si - Cr
 $Mn/Z \text{ (mol/mol)} = 0.018$, $Si/Z \text{ (mol/mol)} = 0.005$,
 $Z = (Fe + Mn + Si + Cr)$, 950°C, 1 atm



Database: FactPS, Ftoxid, FSstel

Solution phases selected in calculation
BSpinel, BMonoxide, FCC_A1, AOlivine

Compound species selected:
 Cr_2O_3 , SiO_2

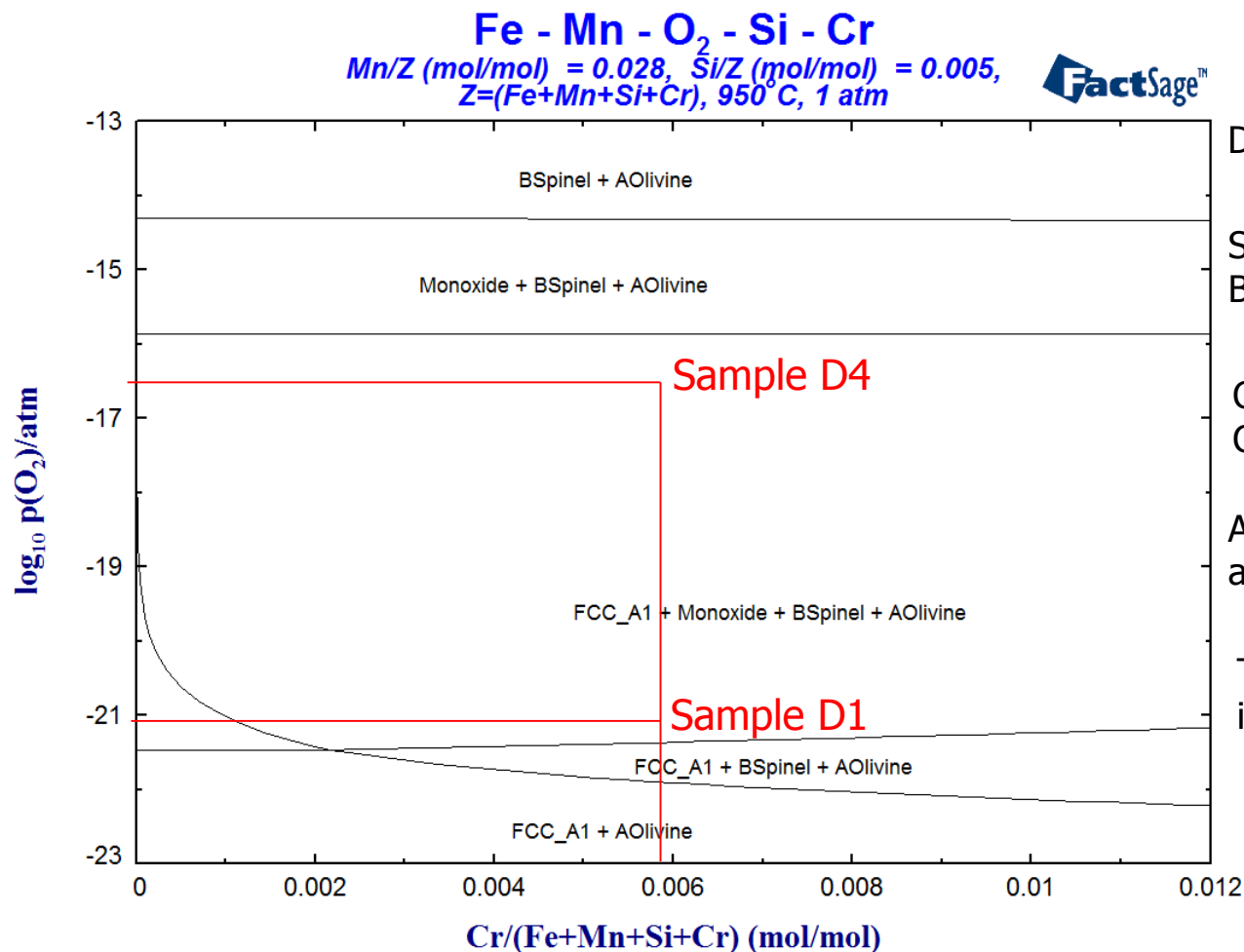
AOlivine phase is a solution of Fe_2SiO_4
and Mn_2SiO_4

The effect of Si is taken into account
in calculation

XRD results agree with "Factsage"
calculation except sample B1, but the
trend is correct

Prediction of oxides formation: Fe-Mn-Cr-Si

Phase diagram of Fe-2.8Mn-0.5Si-Cr alloy in O₂ environment



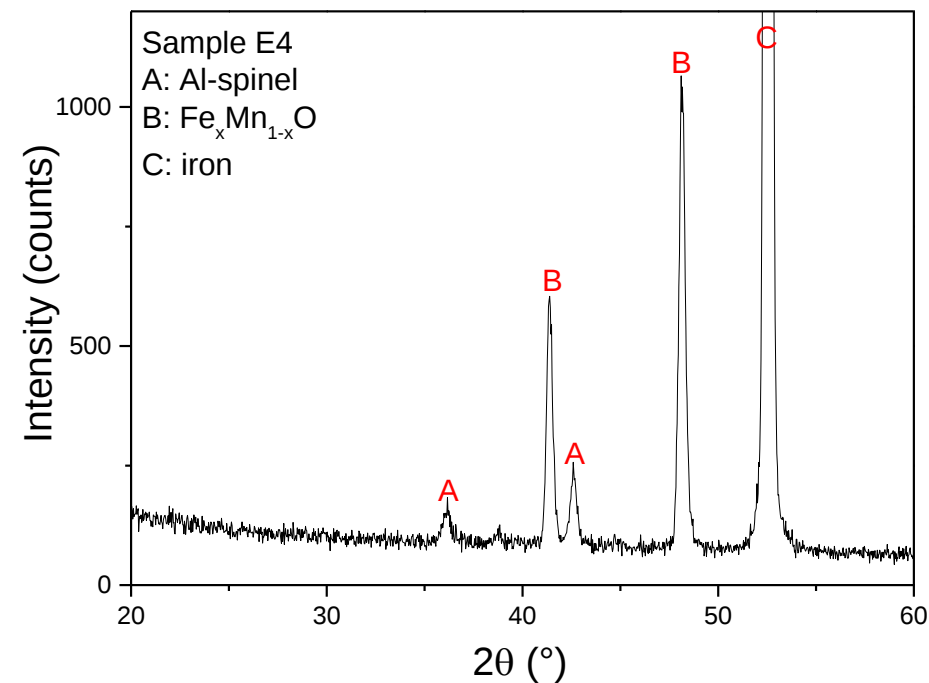
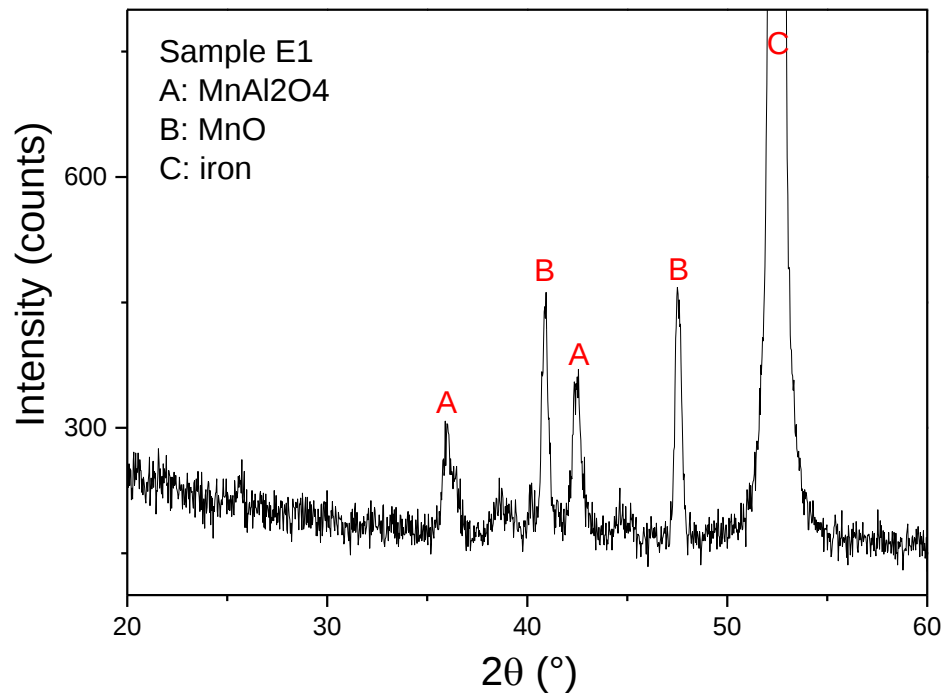
XRD analysis: Fe-Mn-Al-(Si)

Annealing condition in N₂ with 5 vol.% H₂

Sample	Dew point (°C)	Temperature (°C)	P _{O2}
E1	-45	950	8.0×10^{-22}
E4	+10		2.3×10^{-17}

Sample composition (mol%):

	C	Mn	Si	Al
Sample E	0.81	1.8	0.29	1.93



Addition of Al leads to formation of Al-spinel oxide

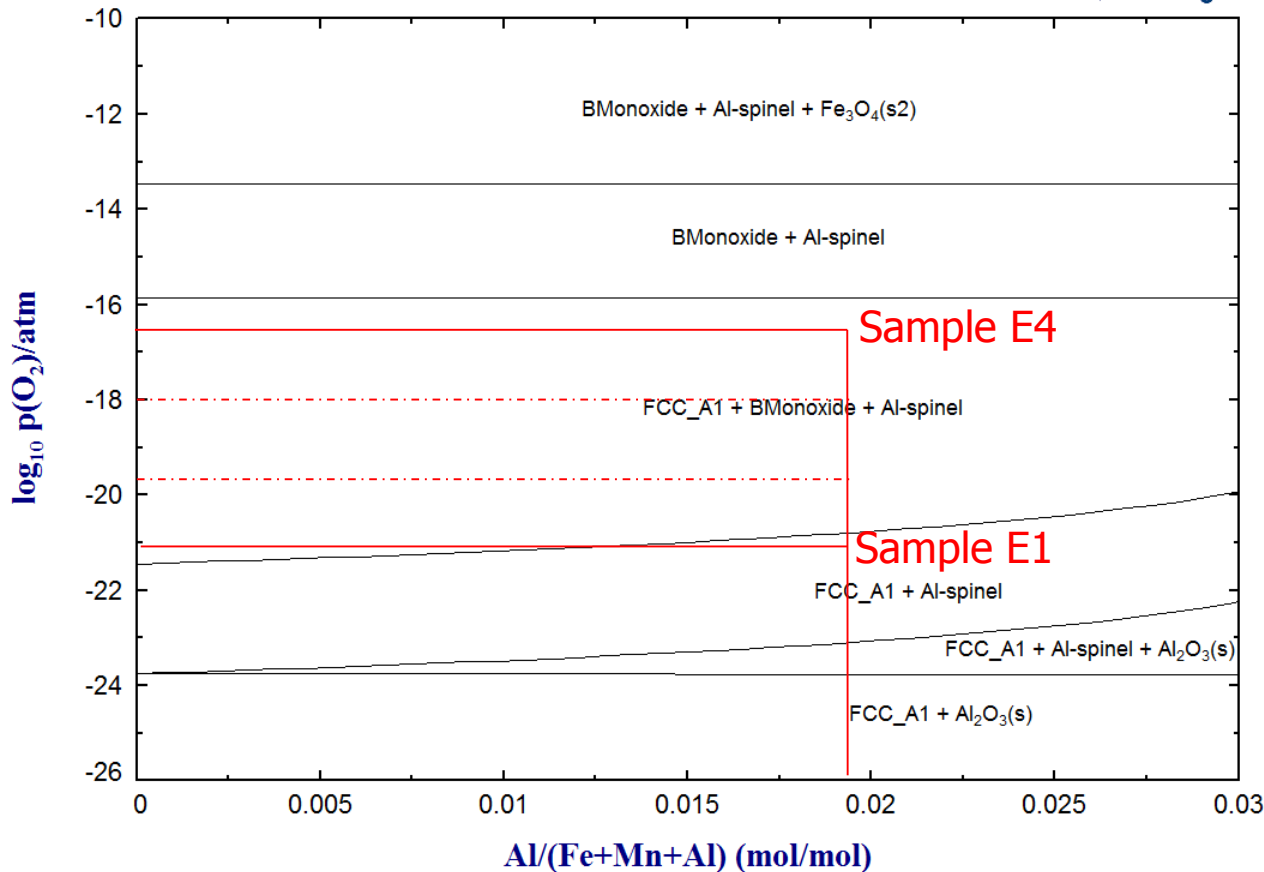
Prediction of oxides formation: Fe-Mn-Al

Phase diagram of Fe-1.8Mn-Al alloy in O₂ environment

O₂ - Fe - Mn - Al
Mn/(Fe+Mn+Al) (mol/mol) = 0.018, 950°C, 1 atm



Database: FactPS, Ftoxid, FSstel



Solution phases selected in calculation:
Al-spinel, BMonoxide, FCC_A1

Compound species selected in calculation:
Fe₃O₄, Al₂O₃, MnAl₂O₄, Al₂Fe₂O₆,
FeAl₂O₄, Al₂Fe₂O₆

Al-spinel is a solution of only FeAl₂O₄,
MnAl₂O₄, Al₈O₁₂

For sample E1 only Al-spinel oxide is predicted

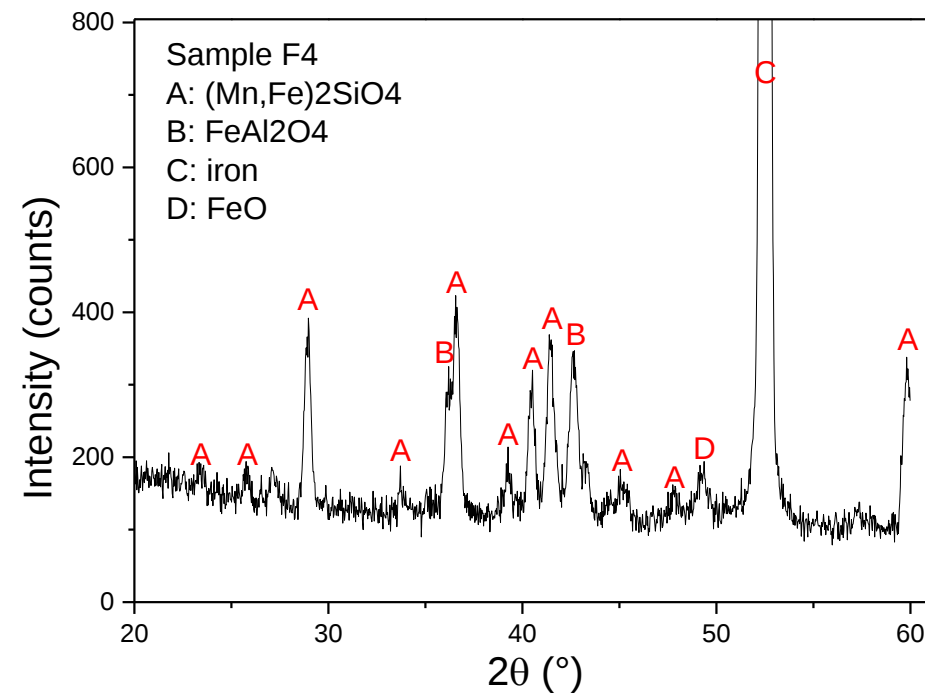
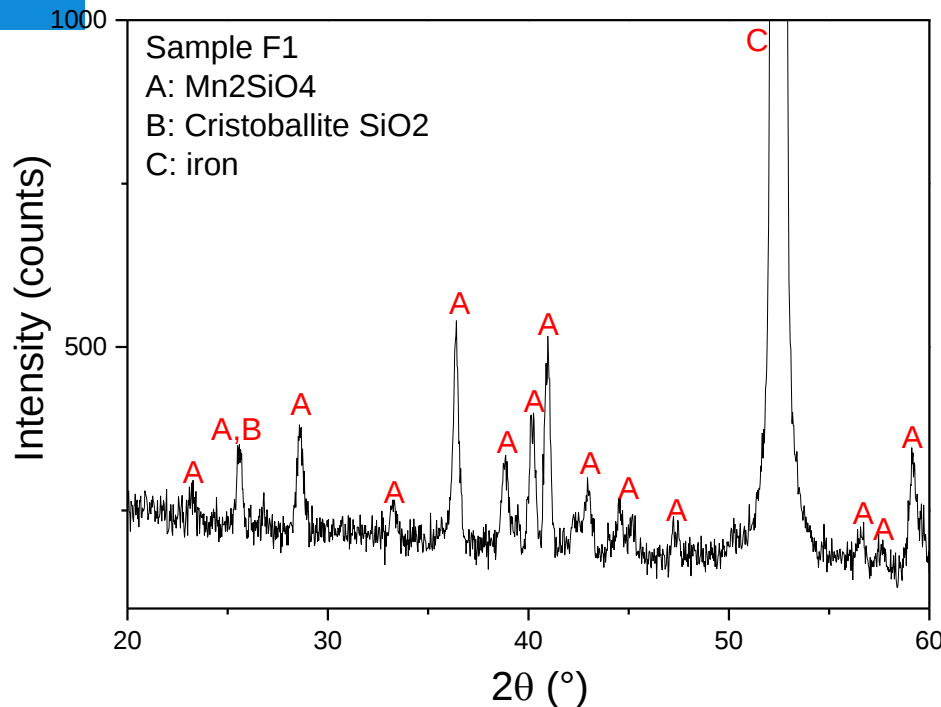
XRD analysis: Fe-Mn-Al-Si

Annealing condition in N₂ with 5 vol.% H₂

Sample	Dew point (°C)	Temperature (°C)	P _{O2}
F1	-45	950	8.0×10 ⁻²²
F4	+10		2.3×10 ⁻¹⁷

Sample composition (mol%):

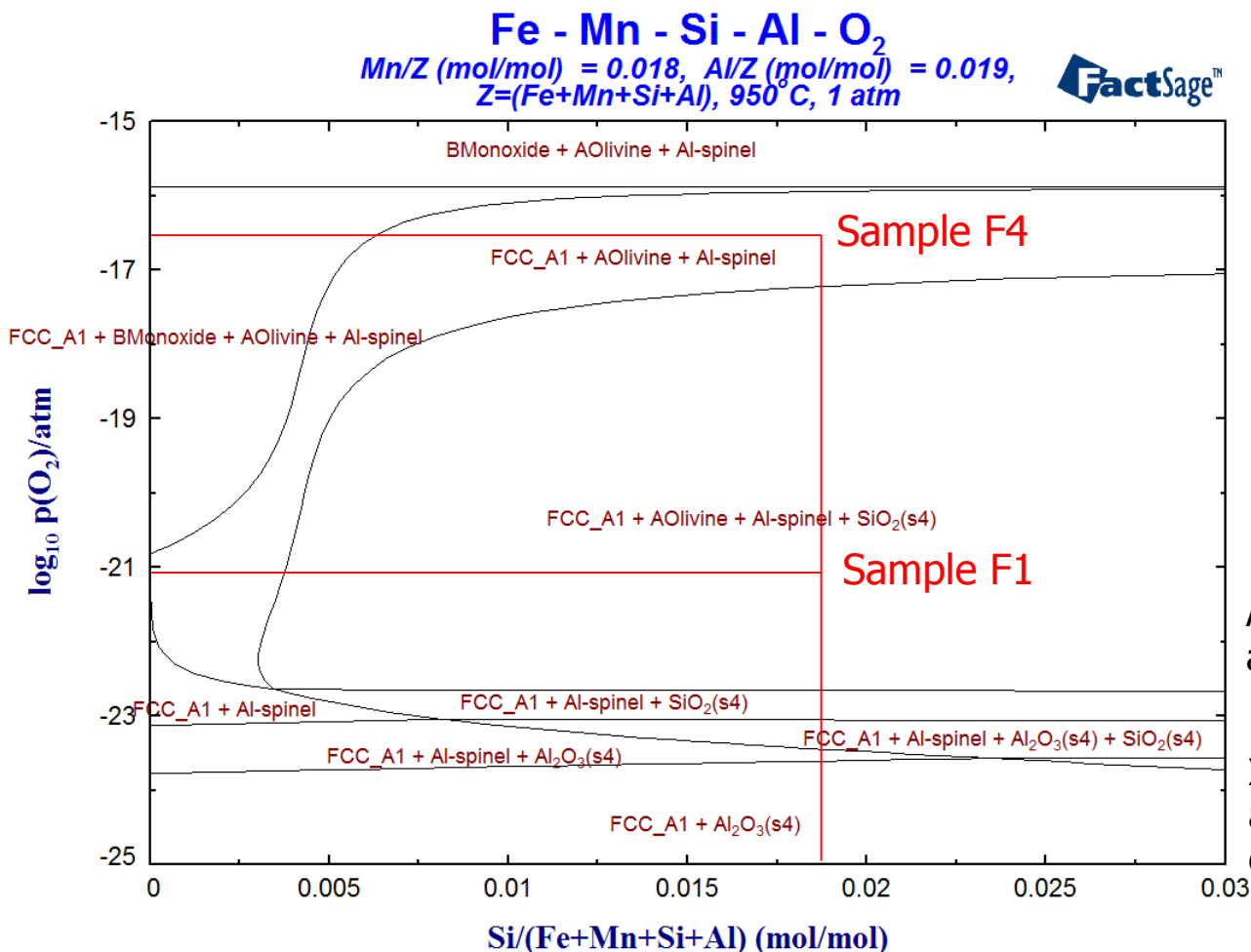
	C	Mn	Si	Al
Sample F	0.91	1.78	1.88	1.81



Addition of Si and Al leads to the formation of Mn₂SiO₄ and Al-spinel oxide, respectively
MnO is not formed

Prediction of oxides formation: Fe-Mn-Al-Si

Phase diagram of Fe-1.8Mn-Si-1.9Al alloy in O₂ environment



Database: FactPS, Ftoxid, FSstel

Solution phases selected in calculation:
Al-spinel, BMonoxide, FCC_A1, AOlivine

Compound species selected:
SiO₂, Al₂O₃ from Ftoxid

AOlivine phase is a solution of Fe₂SiO₄ and Mn₂SiO₄

XRD results are generally in agreement with "Factsage" calculation

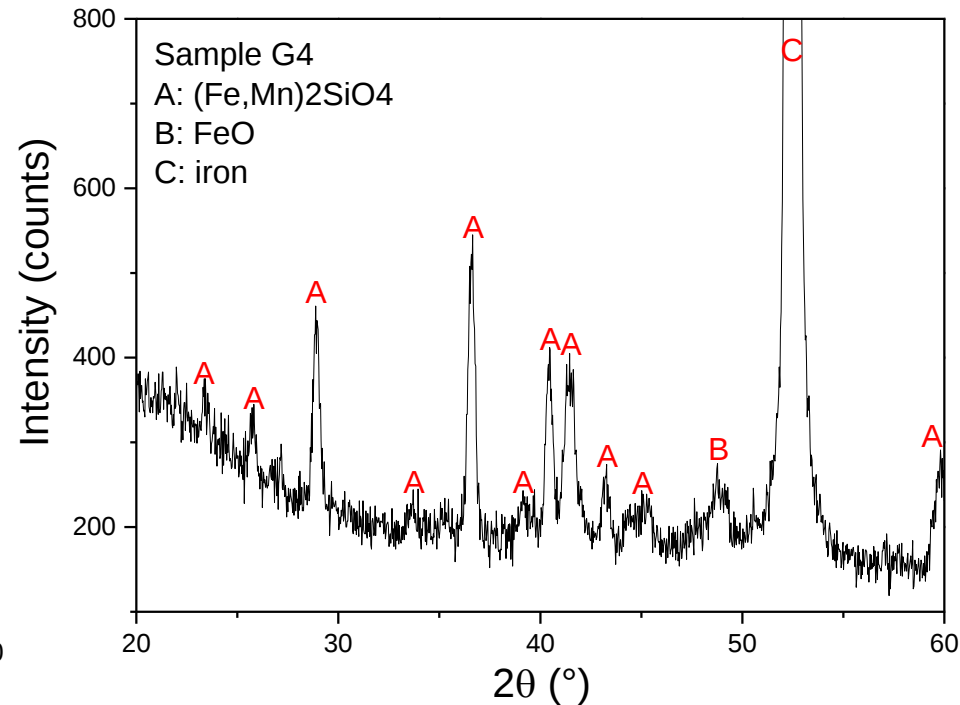
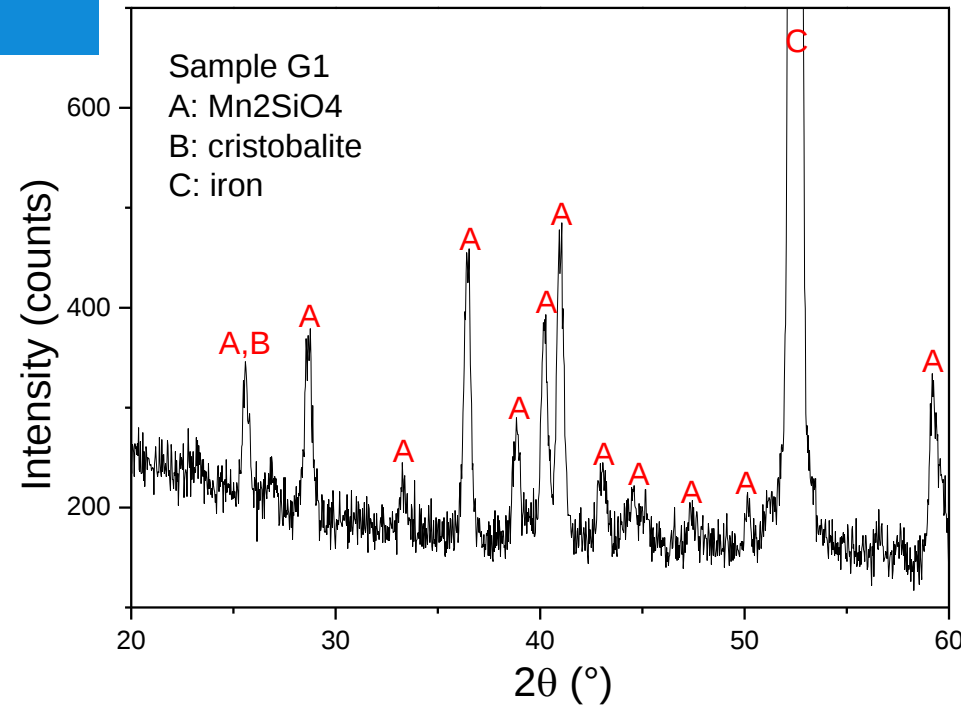
XRD analysis: Fe-Mn-Si

Annealing condition in N₂ with 5 vol.% H₂

Sample	Dew point (°C)	Temperature (°C)	P _{O2}
G1	-45	950	8.0×10^{-22}
G4	+10		2.3×10^{-17}

Sample composition (mol%):

	C	Mn	Si	Al
Sample G	0.48	1.91	1.84	0.03



Si leads to formation of Mn₂SiO₄, and diffraction peaks of Mn₂SiO₄ shift to the right with increasing dew point

MnO is not formed

Prediction of oxides formation: Fe-Mn-Si

Phase diagram of Fe-1.8Mn-Si alloy in O₂ environment

Database: FactPS, Ftoxid, FSstel

O₂ - Fe - Mn - Si
Mn/(Fe+Mn+Si) (mol/mol) = 0.018, 950°C, 1 atm



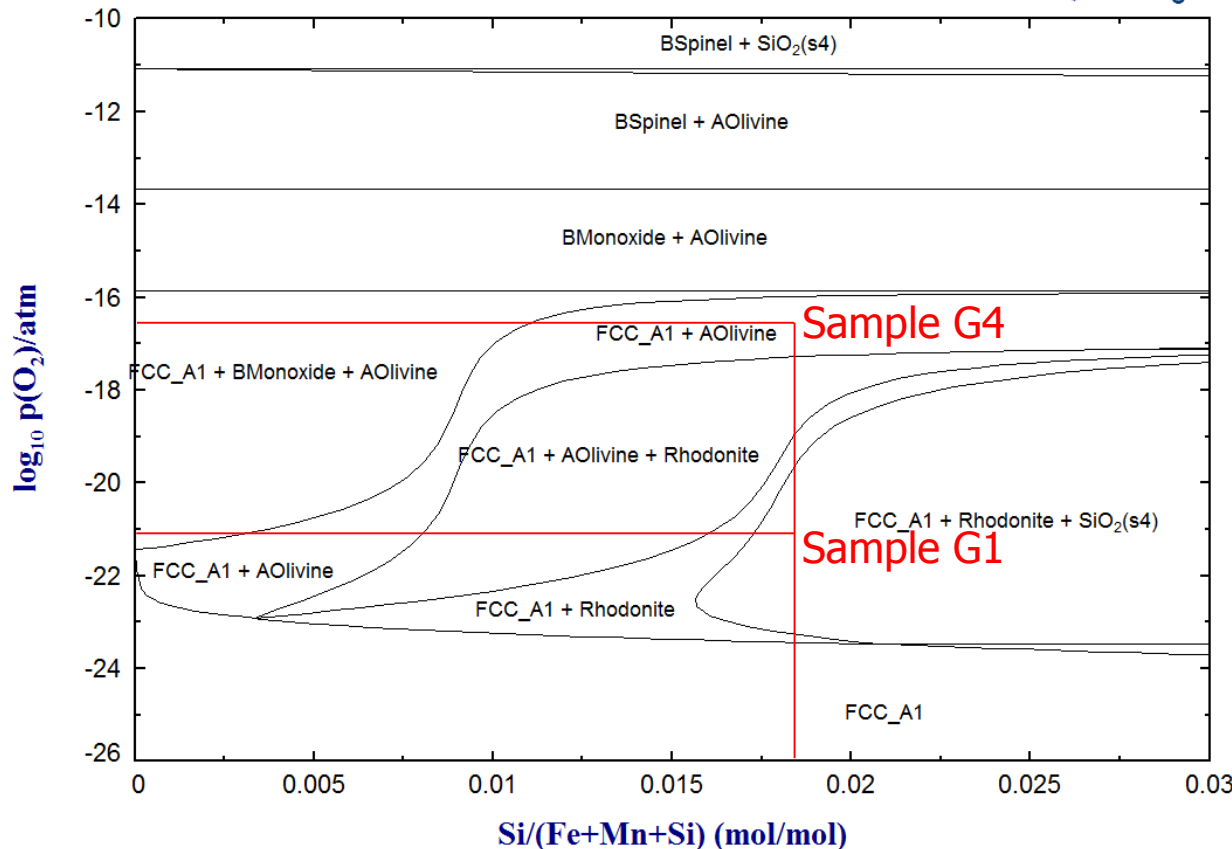
Solution phases selected in calculation:
BSpinel, BMonoxide, FCC_A1, AOlivine, Rhodonite

Pure solid phases selected in calculation:
SiO₂, MnSiO₃, Mn₂SiO₄, FeSiO₃, Fe₂SiO₄, Mn₂O₃

AOlivine phase is a solution of Fe₂SiO₄ and Mn₂SiO₄

Rhodonite phase is a solution of MnSiO₃ and FeSiO₃

"Factsage" calculation also predicts Rhodonite, but it may not be formed due to kinetic reasons



Summary

- Oxidation mode changes from external oxidation to internal oxidation with increasing dew point (from -45 to +10 ° C)
- In Fe-Mn binary steel, the internal oxides formed are uniformly distributed, i.e. no grain boundary effect observed
- Oxides are formed along grain boundaries when Si is added to steel at both low and high dew points
- Oxide precipitates are not uniformly distributed when Si and Al are added to steel
- Al nitrides are formed internally when annealing in N₂ atmosphere; increasing of dew point suppresses formation of Al nitrides
- All oxides identified by XRD analysis are included in thermodynamic database
- Oxides predicted by thermodynamic calculations are generally in agreement with observed oxides

4.

Outlook

Outlook

- Completing analysis and characterization of oxidized multi-element steel alloys (oxide-phase identification, depth-profiles, external/internal oxidation, etc.
- Validating thermodynamic database for the prediction of the oxide formation (binary, ternary and mixed oxides)
- Developing theory to calculate the effect of 3rd elements on oxide precipitation in Fe alloys (solubility, diffusivity, etc)
- Expanding numerical model for selective oxidation: multi-element steel alloys

Contact

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